

Voltage Control in an HVDC System to Share Primary Frequency Control Reserves between Non-Synchronous Areas

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Outline

- 1 Background
- 2 DC-voltage-based control scheme for primary frequency control
- 3 Coordination with secondary frequency control
- 4 Conclusions

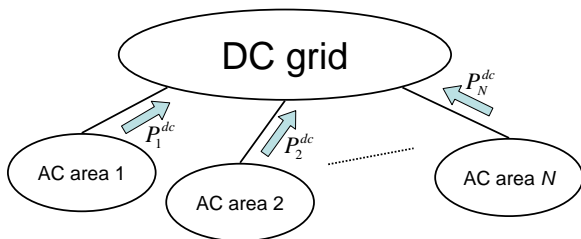
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Primary frequency control

- Frequency control: Limit frequency variations and restore balance between generation and load demand.
- Primary frequency control:
 - Time scale: a few seconds.
 - Based on local frequency measurements.
 - Adjustment of power injections (mainly by generators).
 - Primary reserves: power margins deployable within a few seconds.
- Larger synchronous area:
 - More generators participating in primary frequency control.
 - Lower costs of reserves per MW.
 - Motivation to extend synchronous areas at a continental scale.

Multi-terminal HVDC system



- Generally, P_i^{dc} are supposed to track pre-determined power settings.
- Primary frequency control is independent from one area to another.
- Is it possible to share primary reserves among these AC areas as if they were connected by a large AC grid?

Previous work

- A simple control law:
 - Applied a two-terminal HVDC link.
 - To change the power exchanged via one converter in proportional to the frequency difference between both areas.
 - Generalized by the authors to a multi-terminal HVDC system.
- Problem: Dependency on remote information.
 - reliability
 - delays: potential instability

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Reference Operating Point

- The steady state, at which the system is expected to be operated in the absence of power imbalances. The values are denoted by a bar overhead.
- For each AC area:
 - Frequency: at its nominal value. $\bar{f} = f_{nom}$
 - Aggregated generator:
 - Constant rotational speed: $\bar{P}_e = \bar{P}_m$
 - Electrical output: $\bar{P}_e = \bar{P}_{load} + \bar{P}^{dc}$
 - Mechanical input: equal to its reference value given by the secondary frequency controller: $\bar{P}_m = P_m^o$
- DC grid: at a steady-state power flow.

DC-voltage-based control scheme for an HVDC grid

- Control objective: Sharing primary frequency reserves among non-synchronous areas by **making the frequency deviations stay close to each other.**
- Control variables: $V_1^{dc}, \dots, V_N^{dc}$
- Subcontroller for area i controls V_i^{dc} such that

$$V_i^{dc} = \bar{V}_i^{dc} + \alpha_i(f_i - \bar{f}_i)$$

- where
 - \bar{V}_i^{dc} : Value of V_i^{dc} at the Reference Operating Point.
 - α_i : **controller gain.**
 - f_i : **Frequency of area i .**
 - \bar{f}_i : **Value of f_i at the Reference Operating Point.**

Features

$$V_i^{dc} = \bar{V}_i^{dc} + \alpha_i(f_i - \bar{f}_i)$$

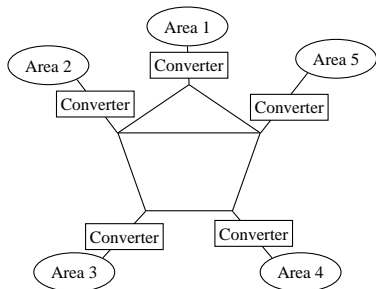
- Idea:
 - ① A positive power imbalance (surplus) in area i : $f_i \uparrow$.
 - ② The control law: $V_i^{dc} \uparrow$.
 - ③ The DC load flow equation: $P_i^{dc} \uparrow$.
 - ④ The positive power imbalance within area i is mitigated: $f_i \downarrow$.
- Decentralized: Each area acts only based on local information. Each area is controlled in the same way.
- The HVDC system functioning in non-conventional mode.

Theoretical results on system stability

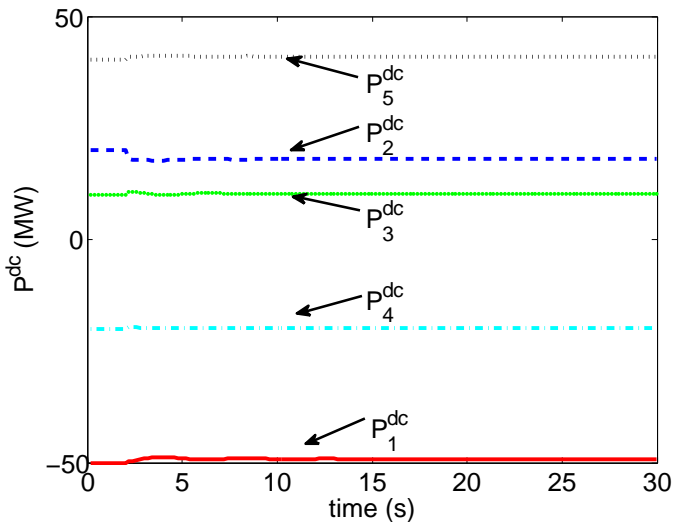
- Assumptions:
 - Linearized model.
 - Identical control gain for each converter.
 - DC power flow approximation.
- Expression of the unique equilibrium point: The frequency deviations are different from each other.
- For the special case of homogeneous AC areas:
 - Asymptotic stability proved: The system converges to the equilibrium point.
 - Effectiveness: By increasing the value of the controller gain α , the differences between the frequency deviations of the AC areas can be made arbitrarily small.

Illustrative case

- An MT-HVDC system with 5 areas: Each area is modeled by an aggregated generator and an aggregated load.
- A nonlinear model: without simplifying assumptions made in the theoretical study.
- Power imbalance: a step increase by 5% in the load demand of area 2 at $t = 2s$.



Simulation result: Power injections

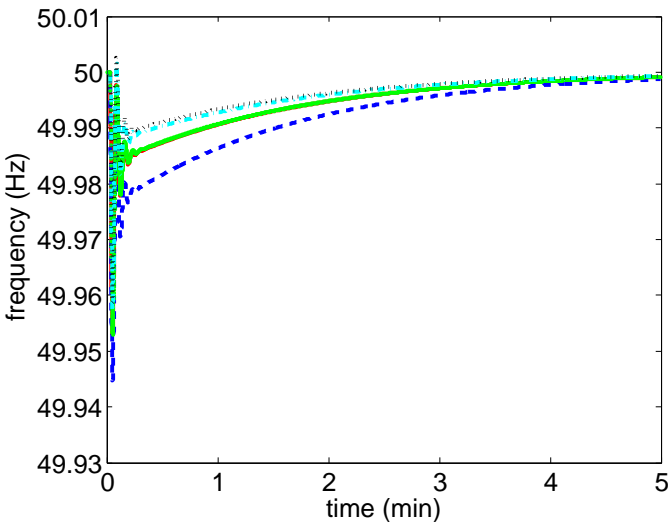


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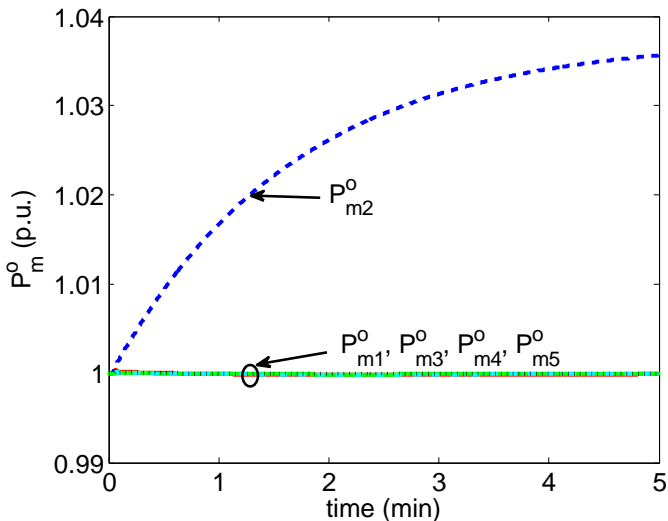
Secondary frequency control

- Objectives: To restore the **frequency** and the **power exchanged between the control areas** back to their nominal/schedule values.
- UCTE practice:
 - Network power frequency characteristic.
 - Area control error (ACE): allows locating the power imbalance.
 - P_m^o is adjusted by an integral controller.
- Direct generalization of the UCTE practice to the HVDC system applying the control scheme for primary frequency control.

Simulation result: Frequency



Simulation result: control variables P_m^o in p.u.



Conclusions

- A control scheme acting on HVDC converters' DC voltage.
- Theoretical results:
 - Expression of the unique equilibrium point.
 - Stability proved for the special case of homogeneous AC areas.
 - Effectiveness of the control scheme demonstrated.
- Simulation results:
 - Frequency deviation mitigated.
 - Use of a non-linear model confirms the theoretical results.
- Secondary frequency control scheme
- Perspectives:
 - Practice: Feasibility of HVDC system with each converter tracking a reference value for its DC voltage.
 - Economic benefits.
 - Integration of wind farms.